# Mechanics of large boulder creation due to wave impacts

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# Aran Islands Project



- Cliff-top storm deposits
- Annually observed boulder movement

- Three islands exposed to Atlantic storms
- Centuries since last tsunami event





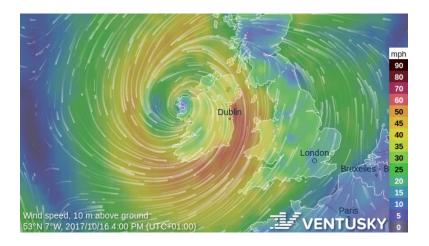


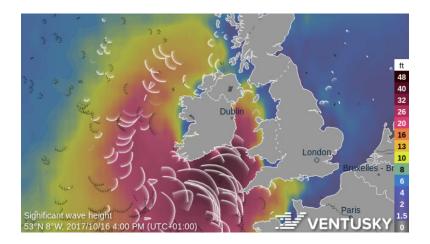
# Extreme Waves



# Extreme Waves







#### Boulder movement

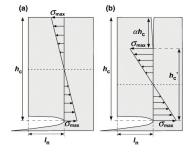
# ...? To be investigated!

#### Question

What happens when waves interact with cliffs?

#### Gravity Loads

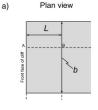
- Notch eroded
- Gravity load stress
- Crack develops
- Load increases
- Cliff collapse



Kogure et al., 2006

#### Wave Loads

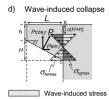
- Gravity & wave load stress
- Stresses pull crack apart
- Cliff collapse





c) Gravity-induced collapse





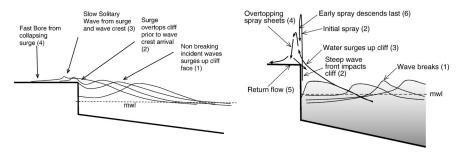


# **Block Erosion**

Wave Impacts & High Pressure Loads  $\rightarrow$  Hydraulic Fracture

- Overtopping waves
- Non-breaking wave impact

- Runup jets
- Breaking wave impact



(Hansom et al., 2008)

# Block Erosion Ex 1



 $\begin{array}{ll} \text{dimensions: } 5.7\,\text{m}\,\times\,2.0\,\text{m}\,\times\,0.8\,\text{m} & 16\,\text{m} \text{ above high water} \\ \text{mass: } 22.3\,\text{t} & 166\,\text{m} \text{ inland} \end{array}$ 

# Block Erosion Ex 2



# Block Erosion Ex 3



Hall et al., 2006

blocks are quarried from the cliff surface

Hansom et al., 2008

the waves are capable of overtopping 10–30 m high cliffs and generate cliff-top forces sufficient to fracture bedrock and to detach and lift boulders as large as  $277 \text{ m}^3$ 

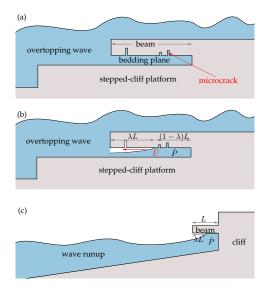
#### Fichaut & Suanez, 2011

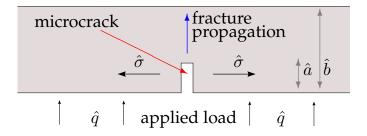
[overtopping] is also capable of quarrying blocks from the cliff face close to the edge and from rock steps on the cliff top, promoting further rock fracturing

#### Erdmann et al., 2017

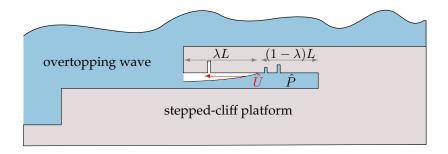
Stratified limestone bedrock with bedding planes and joint patterns allows strong wave fracturing into platy boulders, deposited in ridges .... Those broken from bedrock are platy from limestone strata with constant thickness

# Setup: Exposed Beams

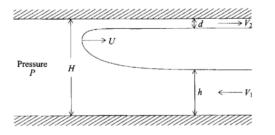




- Normal load from fluid
- Load induces bending stress
- Stress amplified in cracks and weaknesses
- Cracks propagate to complete fracture



- Dynamics of crack filling determines load
- Fluid rushes in and fills from inside out

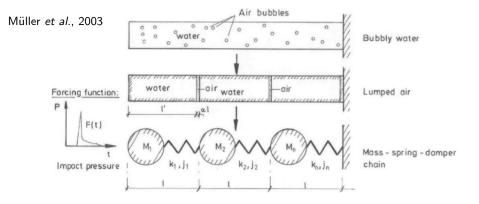


Peregrine & Kalliadasis, 1996

$$P = \frac{V_1^2 k^2}{1 - k^2} \qquad k = \sqrt{h/H}$$
$$U = \frac{V_1 k^2}{1 - k^2}$$

# **Filling Flows**

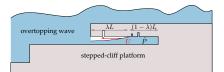
Full air/water mixtures propagate pressure pulses when further impacts occur



#### Assumptions

- Piecewise spatially constant load fraction  $\lambda$  unfilled
- Neglect gravity load
- Quasi-static
- Euler-Bernoulli & Timoshenko beam theories
- Griffith Theory for Mode I brittle fracture

$$q = egin{cases} 0 & 0 < x < \lambda \ P(1-\lambda) & \lambda \leq x < 1 \end{cases}$$



# Deformation

#### Euler-Bernoulli

$$(u_x, u_y, u_z) = (0, 0, w(x))$$
  
 $\frac{\partial^4 w}{\partial x^4} = \alpha^2 q$ 

#### Timoshenko

(

$$u_{x}, u_{y}, u_{z}) = (-z\phi(x), 0, w(x))$$
$$\frac{\partial^{3}\phi}{\partial x^{3}} = \alpha^{2}q,$$
$$\frac{\partial w}{\partial x} = \phi - \omega^{2}\frac{\partial^{2}\phi}{\partial x^{2}}$$

$$w(1) = 0,$$
  $\frac{\partial w}{\partial x}(1) = 0,$   
 $\frac{\partial^2 w}{\partial x^2}(0) = 0,$   $\frac{\partial^3 w}{\partial x^3}(0) = 0.$ 

$$w(1) = 0, \quad \phi(1) = 0,$$
  
 $rac{\partial \phi}{\partial x}(0) = 0, \quad -\phi(0) + rac{\partial w}{\partial x}(0) = 0.$ 

 $M = -\frac{\partial^2 w}{\partial x^2} \quad \sigma = \zeta M z \qquad M = -\frac{\partial \phi}{\partial x} \quad \sigma = \zeta M z$  $\alpha^2 = \hat{P} L^4 / \delta E I \qquad \omega^2 = E I / \kappa A G L^2 \qquad \zeta = \delta^2 E / \hat{P}$ 

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# Deformation

#### Euler–Bernoulli

$$w = \begin{cases} \frac{\alpha^2 q}{24} (1-\lambda)^3 (3-4x+\lambda) & 0 < x < \lambda \\ \frac{\alpha^2 q}{24} \left[ (x-\lambda)^4 + (1-\lambda)^3 (3-4x+\lambda) \right] & \lambda \le x < 1 \end{cases}$$

#### Timoshenko

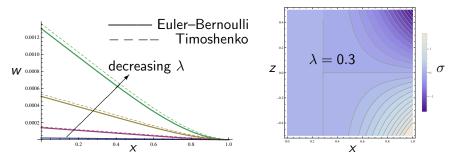
$$\begin{split} \phi &= \begin{cases} \frac{\alpha^2 q}{6} (\lambda - 1)^3 & 0 < x < \lambda \\ \frac{\alpha^2 q}{6} (x - 1) \left[ 1 + x + x^2 - 3\lambda - 3x\lambda + 3\lambda^2 \right] & \lambda \le x < 1 \\ \end{cases} \\ w &= \begin{cases} \frac{\alpha^2 q}{24} (1 - \lambda)^2 \left[ 3 - 4x(1 - \lambda) - 2\lambda - \lambda^2 + 12\omega^2 \right] & 0 < x < \lambda \\ \frac{\alpha^2 q}{24} (1 - x) \left[ 3 - x^3 - x^2(1 - 4\lambda) - 8\lambda + 6\lambda^2 + 12\omega^2 \right] \\ & -24\lambda\omega^2 - x(1 - 4\lambda + 6\lambda^2 - 12\omega^2) \right] & \lambda \le x < 1 \end{cases}$$

#### Euler–Bernoulli & Timoshenko

$$\sigma = \begin{cases} 0 & 0 < x < \lambda \\ -\beta^2 P \frac{(1-\lambda)(x-\lambda)^2 z}{2} & \lambda \le x < 1 \end{cases}$$

$$\beta^2 = \delta L^4 / \textit{Ib} \sim \delta^{-2}$$

Stress



 $p = 0.1 = 1/10 \times \text{Fracture stress} \rightarrow \sigma > 1$ 

### Fracture

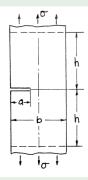
#### Assumptions

- Rock is brittle
- Tensile stress of a Mode I crack

#### Griffith Theory

$$\sigma_{f} = \sqrt{\frac{2E\gamma}{\pi a}} \rightarrow \sqrt{\frac{1-\nu^{2}}{\pi a}} K_{lc}$$
$$\sigma_{c} = \frac{K_{l}}{\sqrt{2\pi r}} f(\theta)$$
$$K_{l} = \sigma \sqrt{\pi a} \sum_{j=0}^{4} S_{j} (a/b)^{j}$$

 $\{S\} = \{ 1.122, -0.231, 10.55, -21.71, 30.382 \}$ 



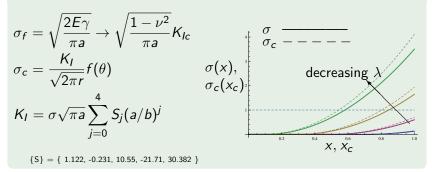
(Tada et al., 1973)

#### Fracture

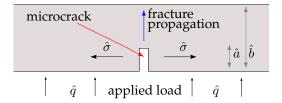
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#### Griffith Theory



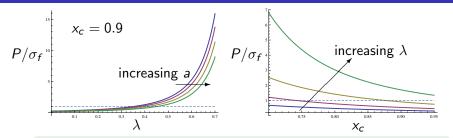
## Pressure for Fracture



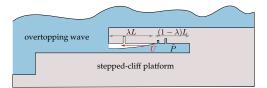
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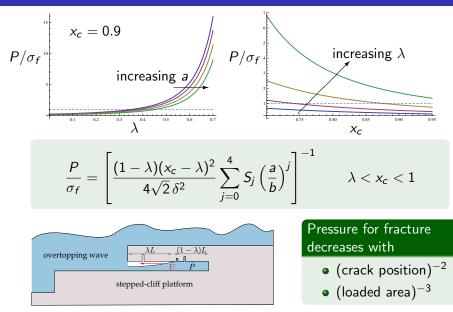
# Pressure for Fracture



$$\frac{P}{\sigma_f} = \left[\frac{(1-\lambda)(x_c-\lambda)^2}{4\sqrt{2}\,\delta^2}\sum_{j=0}^4 S_j\left(\frac{a}{b}\right)^j\right]^{-1} \qquad \lambda < x_c < \infty$$

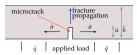


# Pressure for Fracture



# Conclusions







- Simple stressed-beam model for boulder creation via hydraulic fracture
- Pressure for fracture can be significantly below fracture stress
- Boulder creation is a unique way of measuring storm and wave power

