

Simulations of a two-fluid model, sharpening the interface

Rien de Böck
Arris Tijsseling
Barry Koren



Sloshing of Liquefied Natural Gas



Technische Universiteit
Eindhoven
University of Technology



university of
 groningen

UNIVERSITY OF TWENTE.



ANTHONY VEDER



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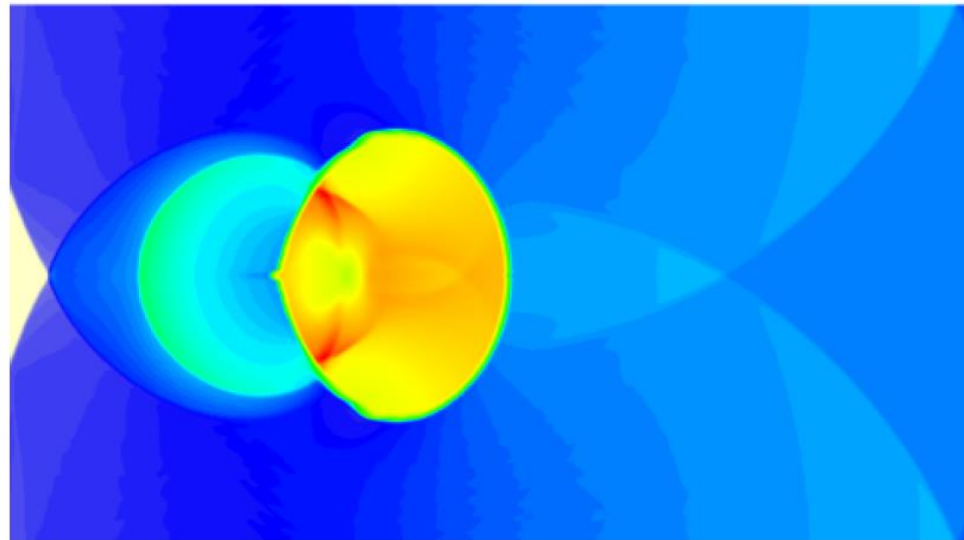
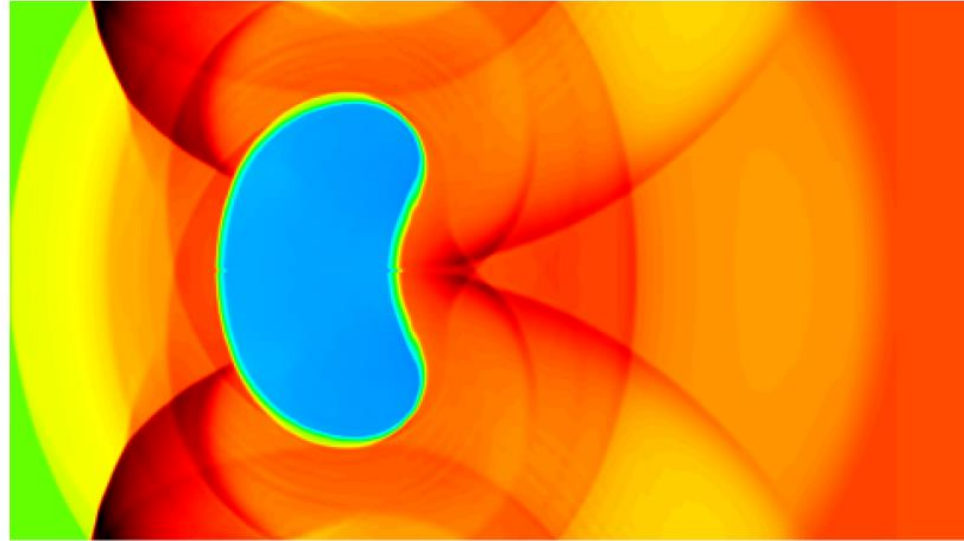


Expert in LNG



CWI

Two-fluid models



Context

Gas and liquid compressibility

Density ratio

Phase transition

Context

Gas and liquid compressibility

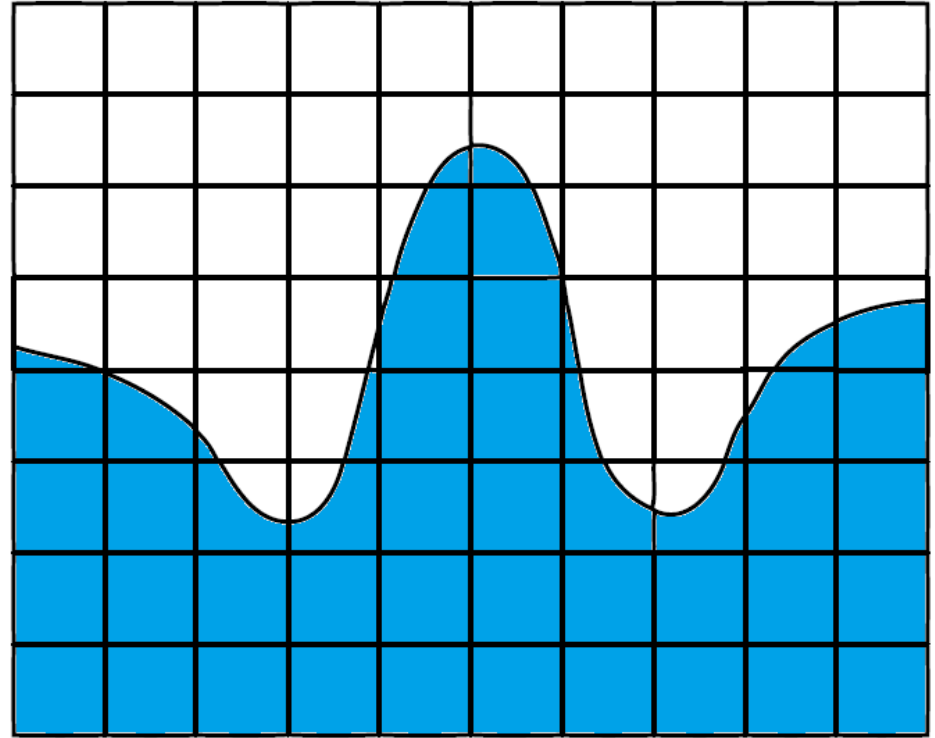
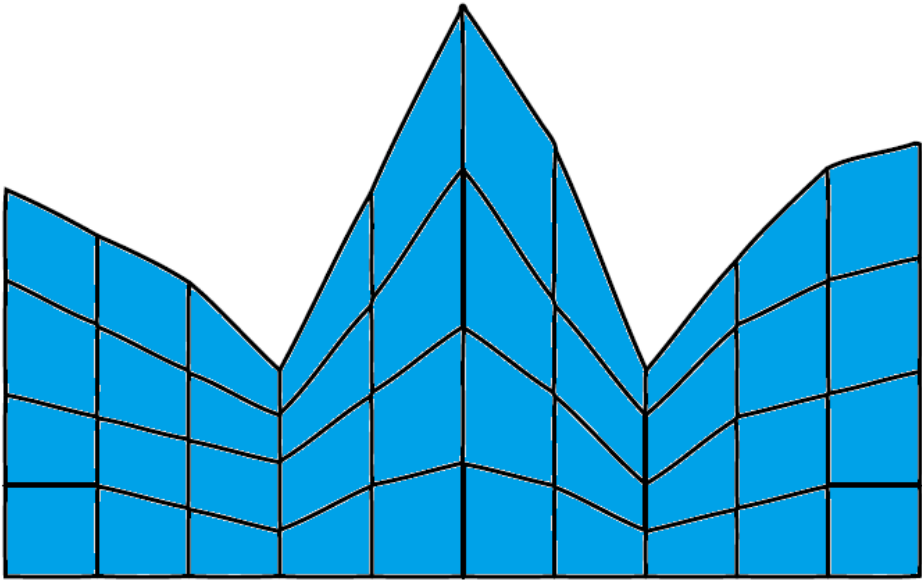
Density ratio

Phase transition

But not

- Surface tension
- Viscosity
- Heat exchange
- Mixing

Two-fluid interfaces



Contents

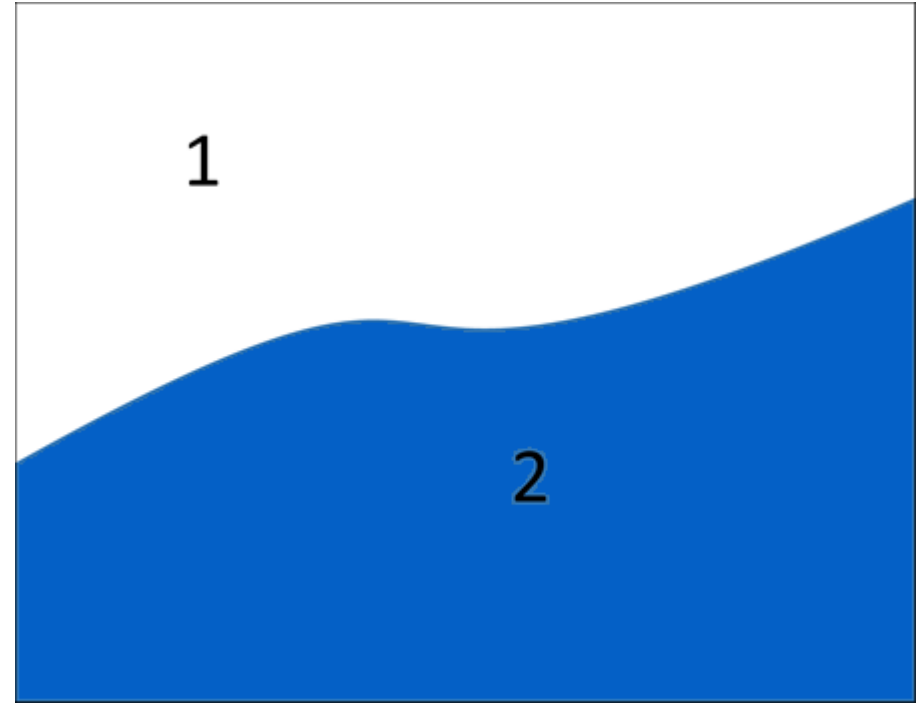
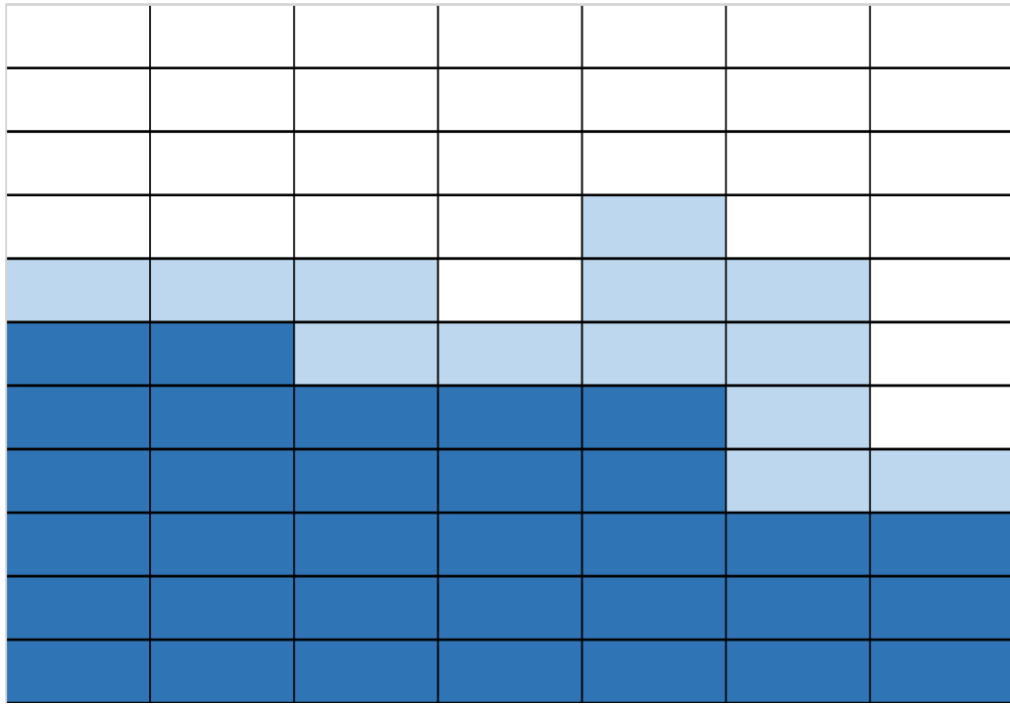
Mathematical model

Numerical method

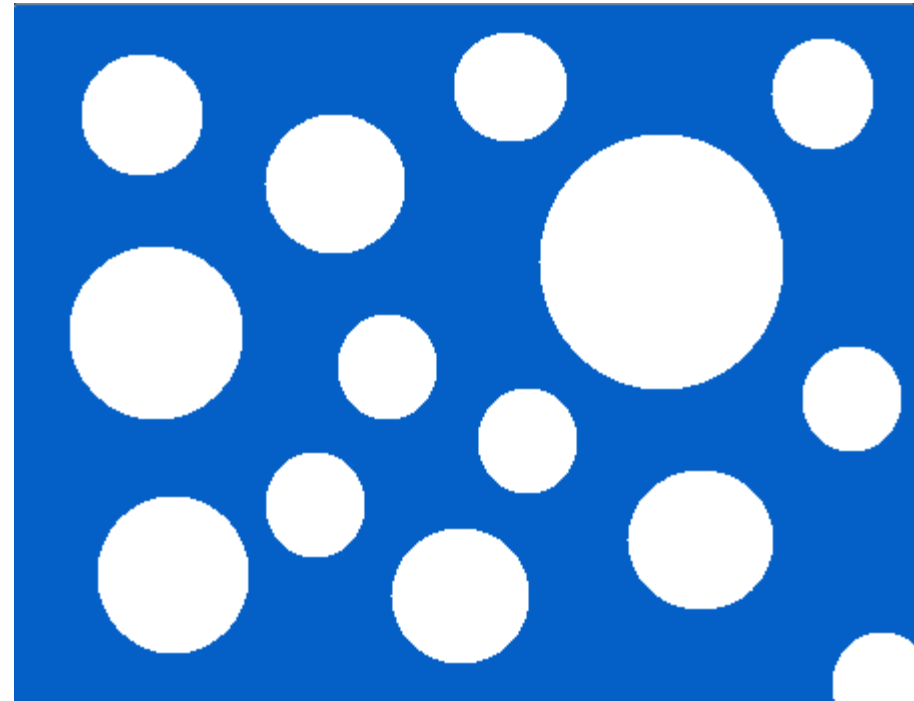
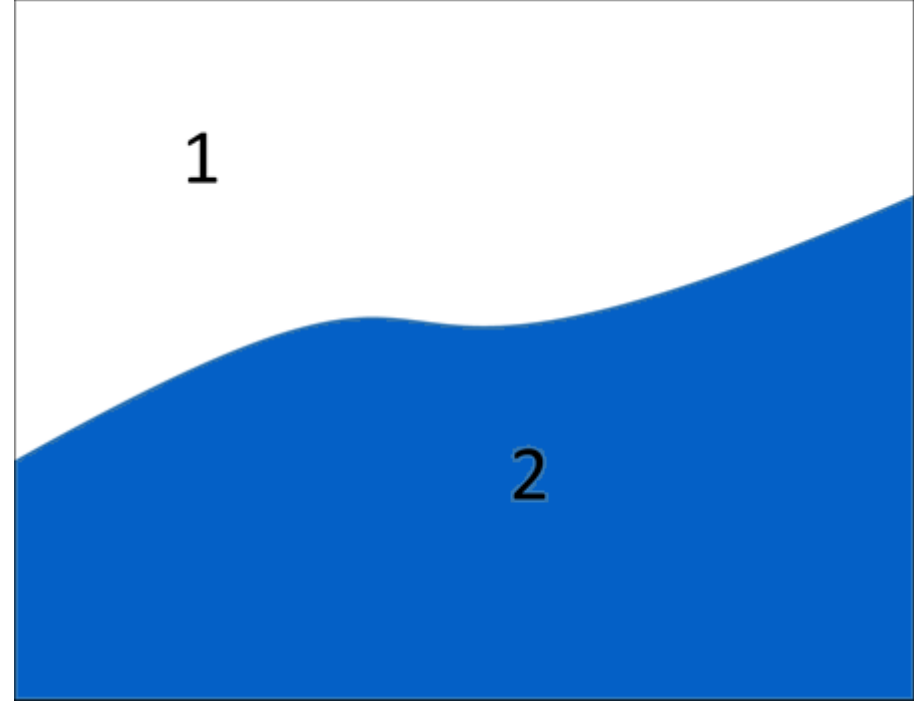
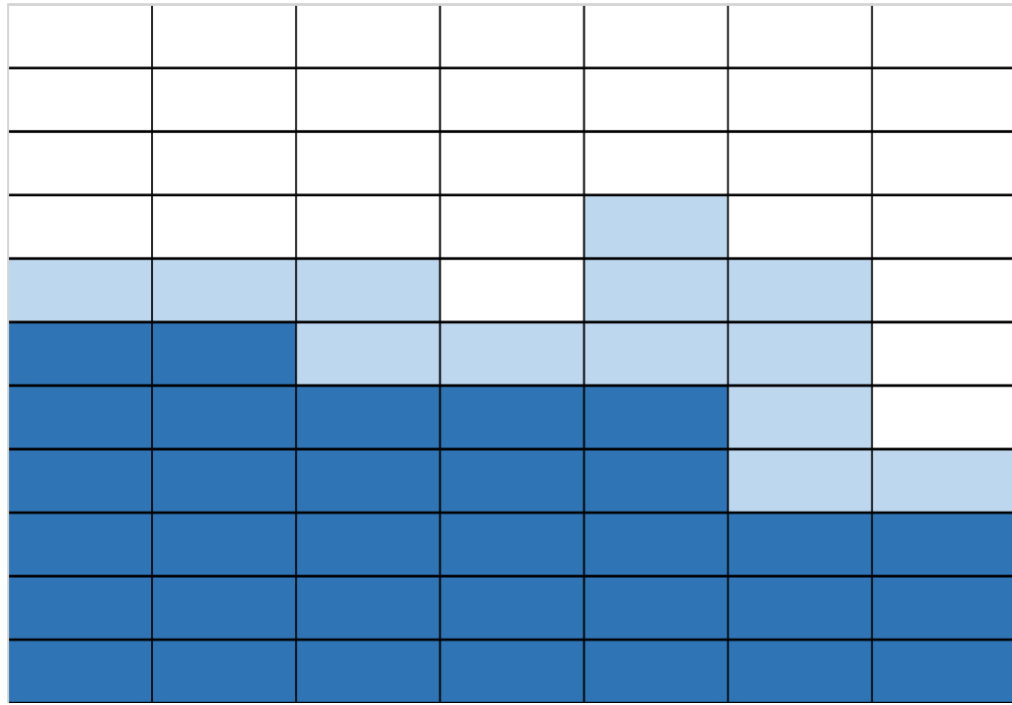
- Spatial reconstruction
- Limiters

Conclusions and future work

The two-fluid model



The two-fluid model

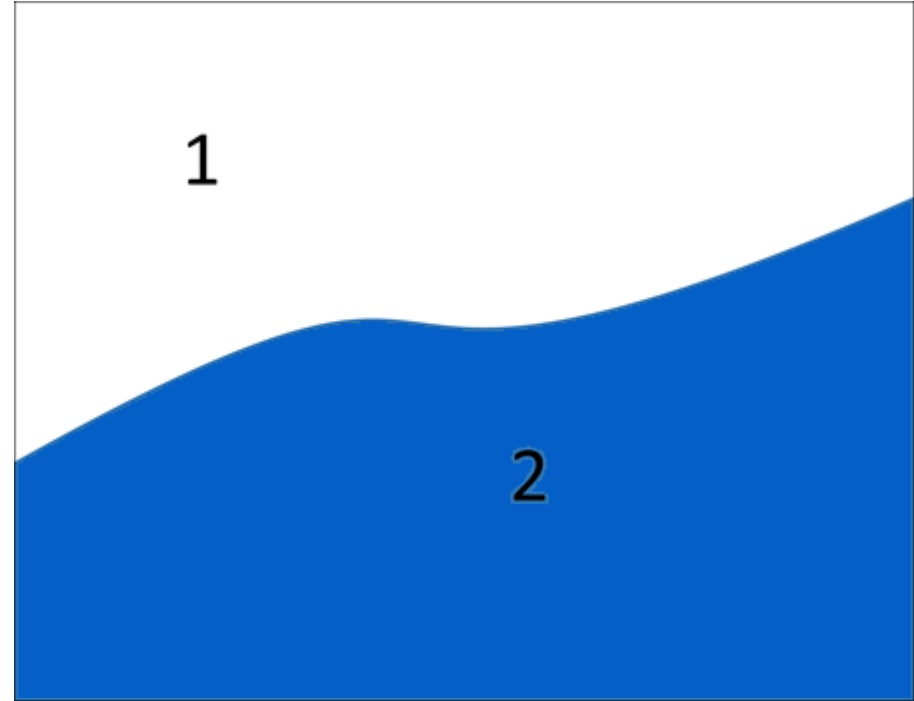


The two-fluid model

Bulk quantities:

$$\rho, u, v, p, e, E$$

Volume fraction α



The two-fluid model

Bulk quantities:

$$\rho, u, v, p, e, E$$

Volume fraction α

Individual quantities:

$$\rho = \alpha\rho_1 + (1 - \alpha)\rho_2,$$

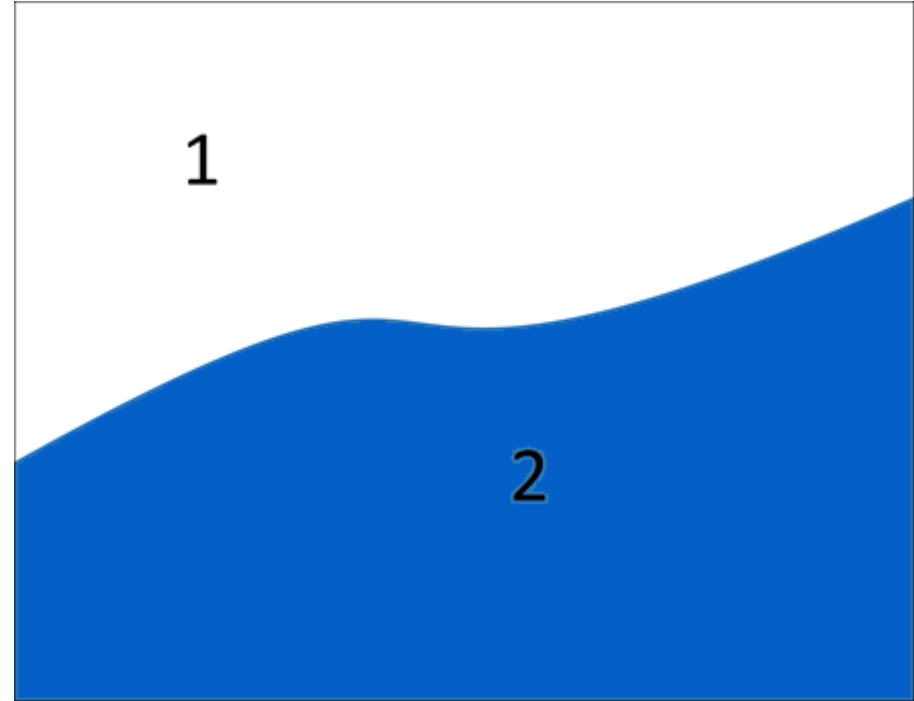
$$u = u_1 = u_2,$$

$$v = v_1 = v_2$$

$$p = p_1 = p_2,$$

$$\rho e = \alpha\rho_1 e_1 + (1 - \alpha)\rho_2 e_2,$$

$$E = e + \frac{1}{2}(u^2 + v^2)$$



The two-fluid model

Bulk mass conservation

$$\rho_t + (\rho u)_x + (\rho v)_y = 0,$$

Bulk momentum conservation

$$(\rho u)_t + (\rho u^2 + p)_x + (\rho uv)_y = 0,$$

$$(\rho v)_t + (\rho uv)_x + (\rho v^2 + p)_y = 0,$$

Bulk energy conservation

$$(\rho E)_t + (u(\rho E + p))_x + (v(\rho E + p))_y = 0,$$

The two-fluid model

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$$(\rho E)_t + (u(\rho E + p))_x + (v(\rho E + p))_y = 0,$$

Mass conservation fluid 1

$$(\alpha \rho_1)_t + (\alpha \rho_1 u)_x + (\alpha \rho_1 v)_y = 0,$$

Advection of volume fraction

$$(\alpha)_t + (\alpha u)_x + (\alpha v)_y = (\alpha - \varphi)(u_x + v_y),$$

The two-fluid model

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Mass conservation fluid 1

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Advection of volume fraction

$$(\alpha)_t + (\alpha u)_x + (\alpha v)_y = (\alpha - \varphi)(u_x + v_y),$$

Parameter φ

$$\varphi = \alpha(1 - \alpha) \frac{\rho_1 c_1^2 - \rho_2 c_2^2}{(1 - \alpha)\rho_1 c_1^2 + \alpha\rho_2 c_2^2},$$

Equations of state

$$e_1 = f(\rho_1, p), e_2 = f(\rho_2, p),$$

The two-fluid model

Hyperbolic System:

Characterics propagate with velocities

$$u - c, u, u + c,$$

$$v - c, v, v + c,$$

c : mixture speed of sound:

$$\frac{1}{\rho c^2} = \frac{\alpha}{\rho_1 c_1^2} + \frac{1 - \alpha}{\rho_2 c_2^2}$$

$$\rho_t + (\rho u)_x + (\rho v)_y = 0,$$

$$(\rho u)_t + (\rho u^2 + p)_x + (\rho uv)_y = 0,$$

$$(\rho v)_t + (\rho uv)_x + (\rho v^2 + p)_y = 0,$$

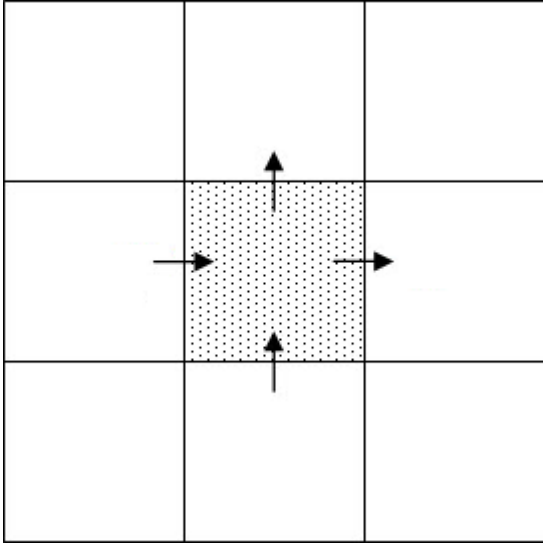
$$(\rho E)_t + (u(\rho E + p))_x + (v(\rho E + p))_y = 0,$$

$$(\alpha \rho_1)_t + (\alpha \rho_1 u)_x + (\alpha \rho_1 v)_y = 0,$$

$$(\alpha)_t + (\alpha u)_x + (\alpha v)_y = (\alpha - \varphi)(u_x + v_y),$$

Numerical method

Finite volume discretization



Basic explicit time step

$$Q_{i,j}^{n+\frac{1}{2}} = Q_{i,j}^n + \frac{\Delta t}{\Delta x} \left(f_{i-\frac{1}{2},j}^n - f_{i+\frac{1}{2},j}^n \right) + \Delta t S_{x,i,j}^n$$

$$Q_{i,j}^{n+1} = Q_{i,j}^{n+\frac{1}{2}} + \frac{\Delta t}{\Delta y} \left(g_{i,j-\frac{1}{2}}^n - g_{i,j+\frac{1}{2}}^n \right) + \Delta t S_{y,i,j}^n$$

$$\rho_t + (\rho u)_x + (\rho v)_y = 0,$$

$$(\rho u)_t + (\rho u^2 + p)_x + (\rho uv)_y = 0,$$

$$(\rho v)_t + (\rho uv)_x + (\rho v^2 + p)_y = 0,$$

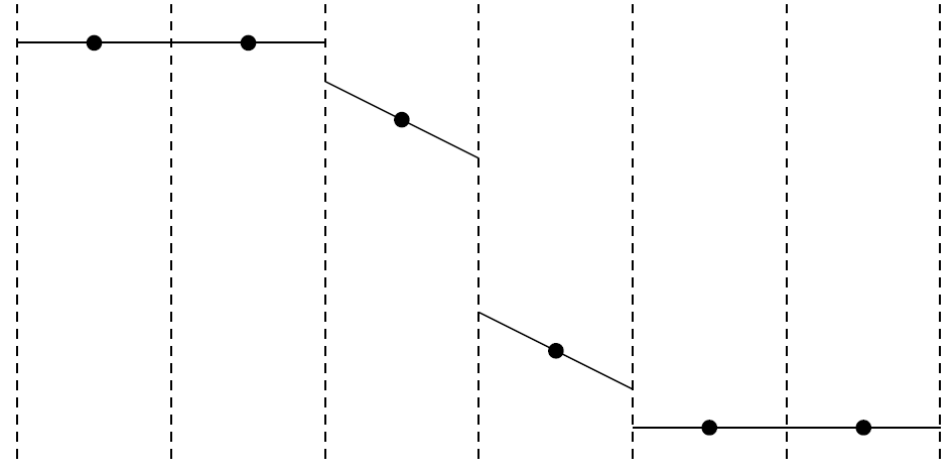
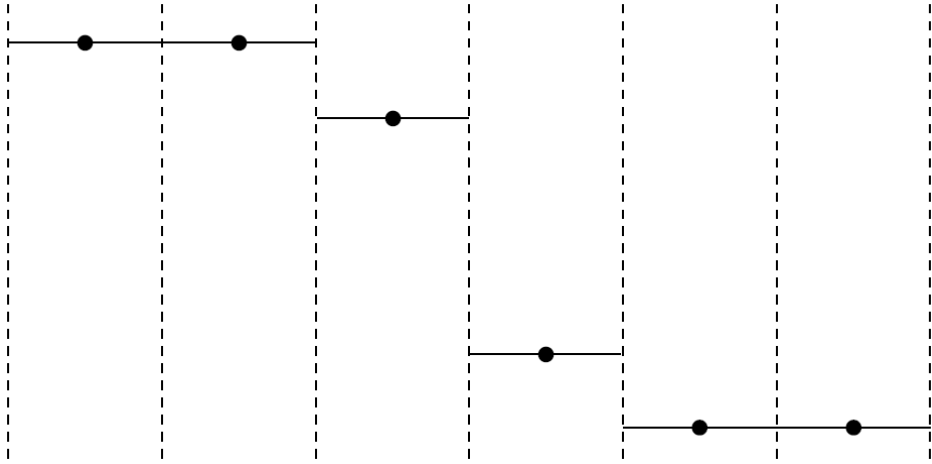
$$(\rho E)_t + (u(\rho E + p))_x + (v(\rho E + p))_y = 0,$$

$$(\alpha \rho_1)_t + (\alpha \rho_1 u)_x + (\alpha \rho_1 v)_y = 0,$$

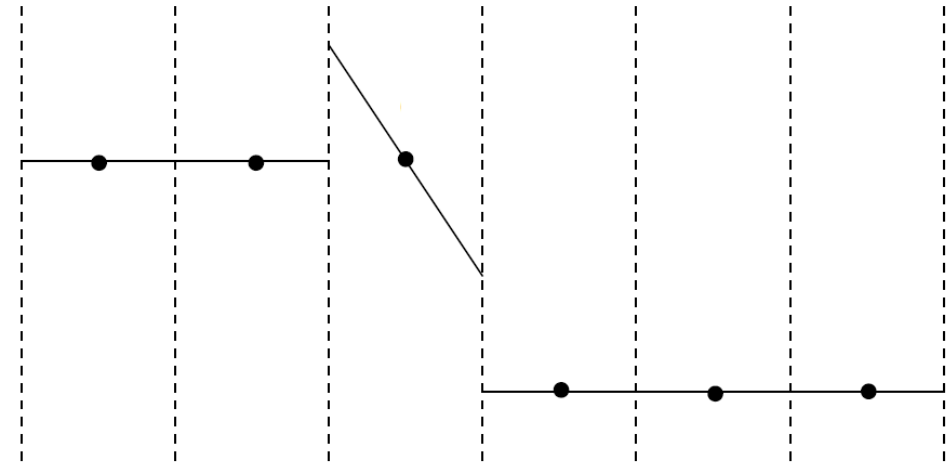
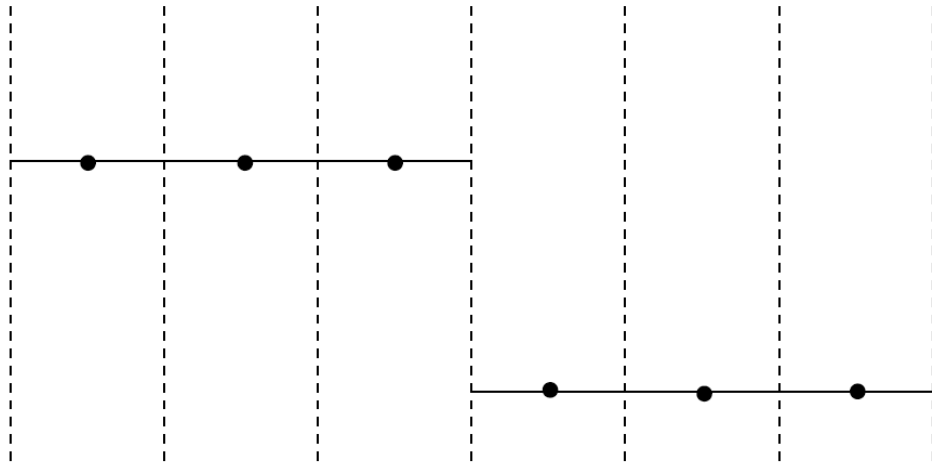
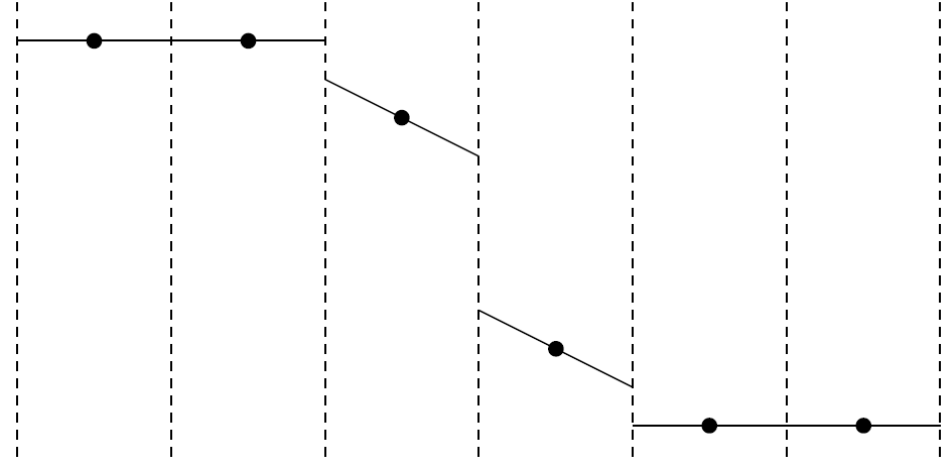
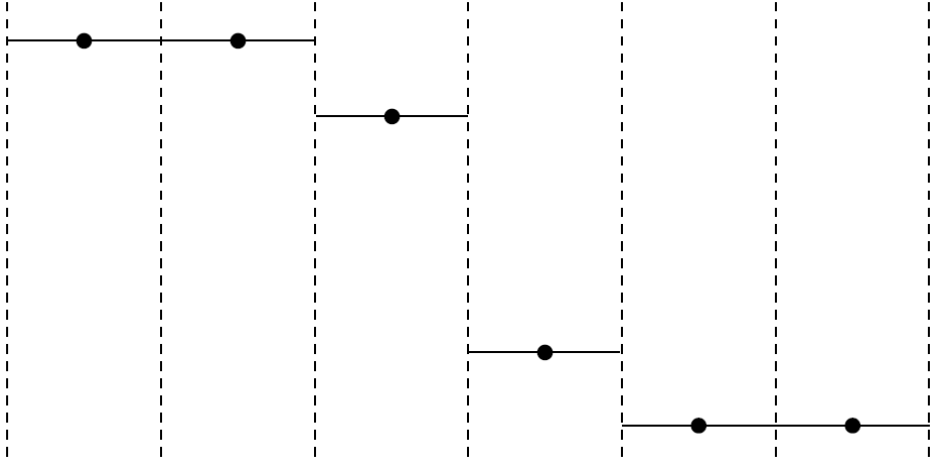
$$(\alpha)_t + (\alpha u)_x + (\alpha v)_y = (\alpha - \varphi)(u_x + v_y),$$

$$Q_t + F(Q)_x + G(Q)_y = S,$$

Spatial reconstruction



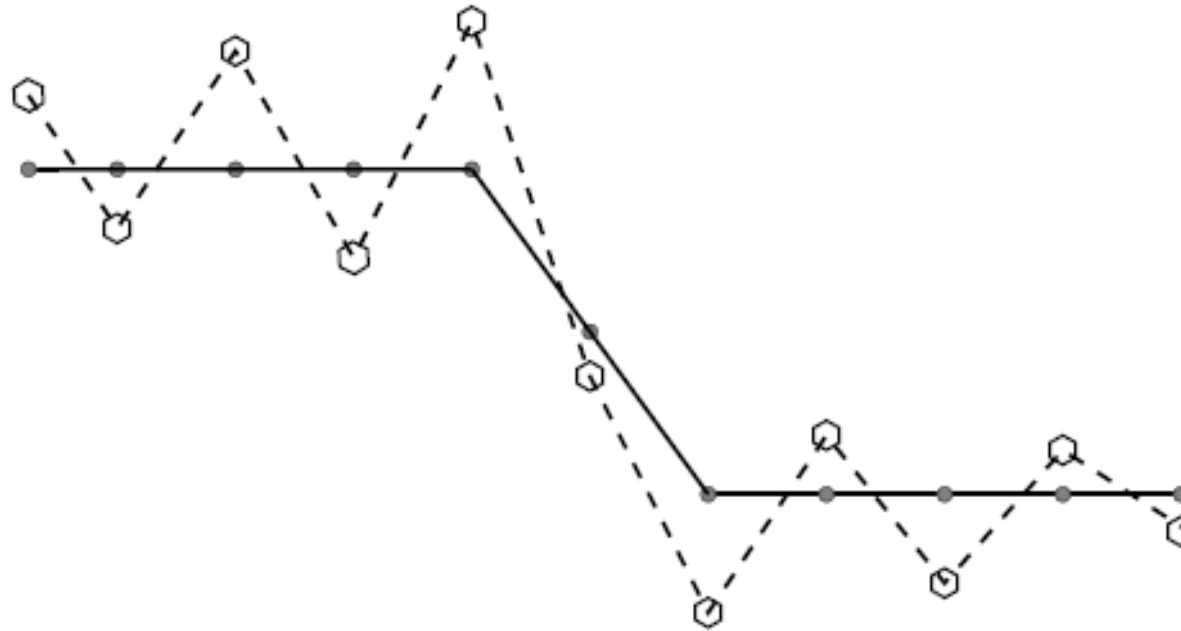
Spatial reconstruction



Spatial reconstruction

TVD schemes

$$TV = \sum_i |q_{i+1} - q_i|$$

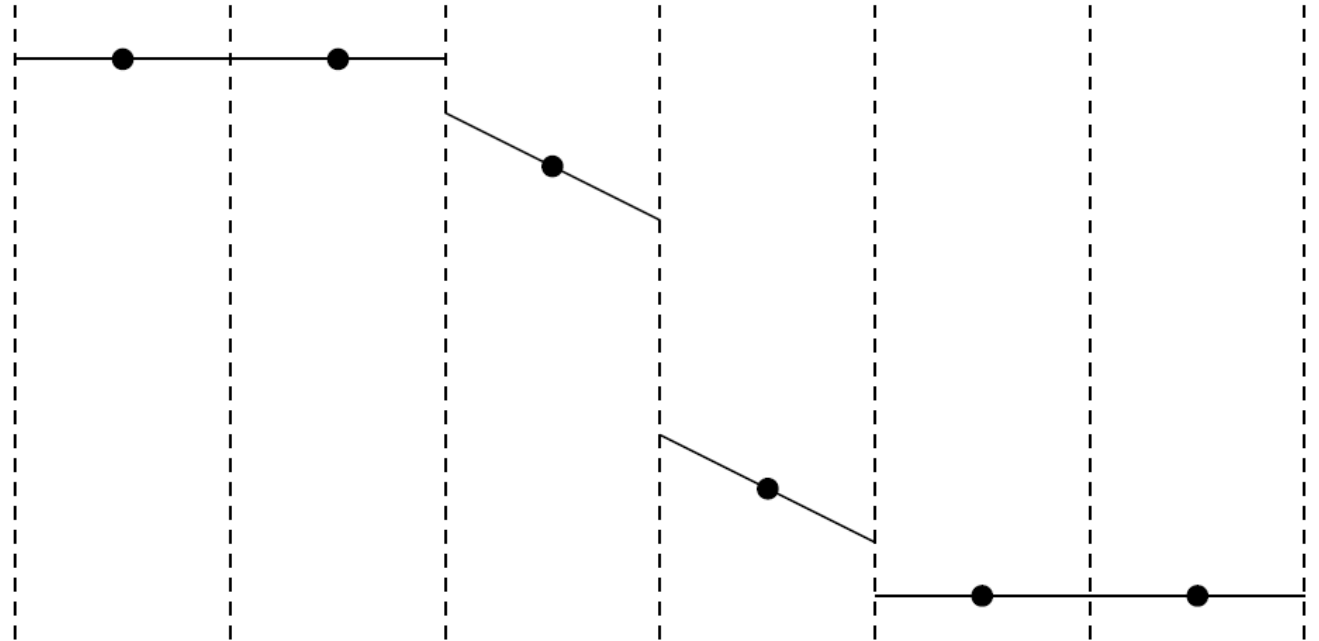


Limiters

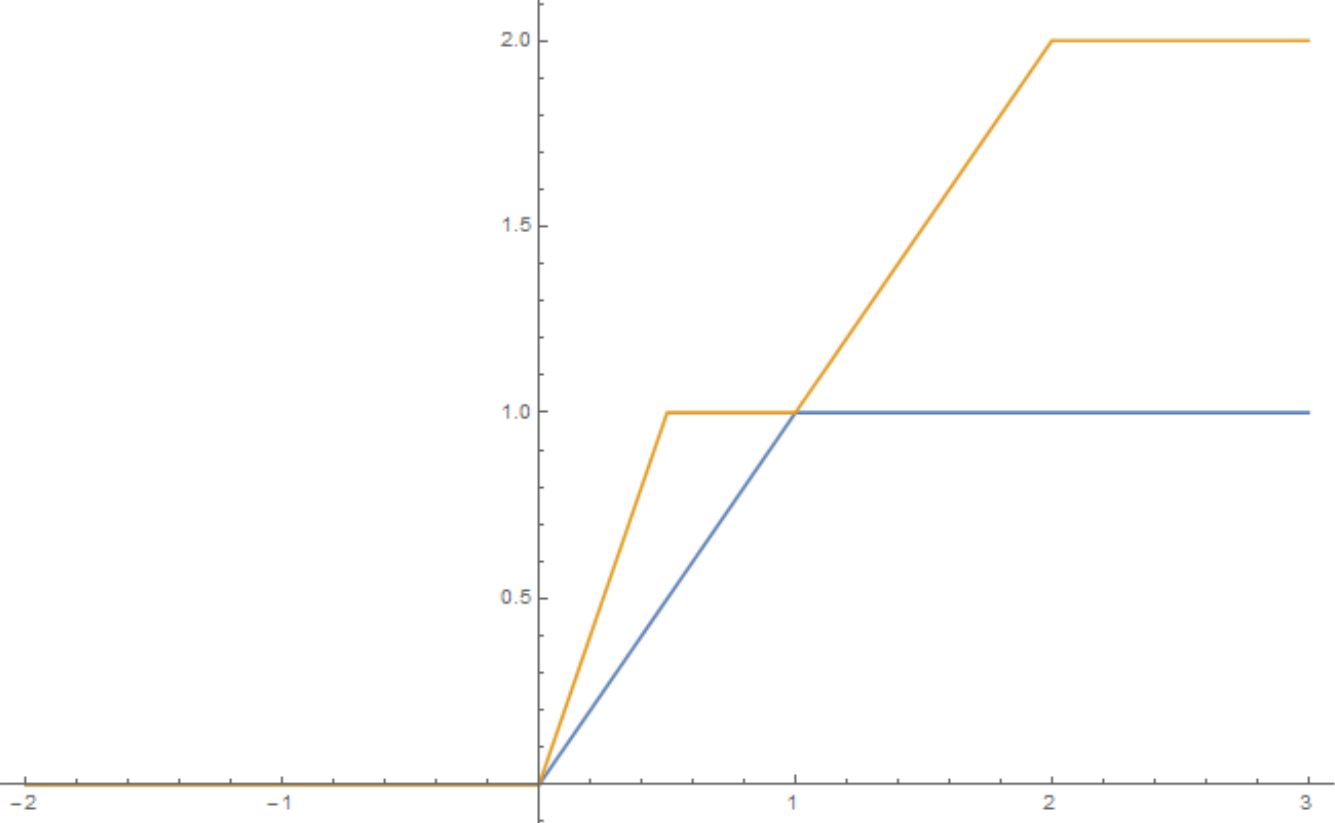
Slope is a function of differences

$$W_{i+\frac{1}{2}}^L = W_i + \frac{1}{2} \psi(r) (W_{i+1} - W_i)$$

$$r = \frac{W_{i+1} - W_i}{W_i - W_{i-1}}$$

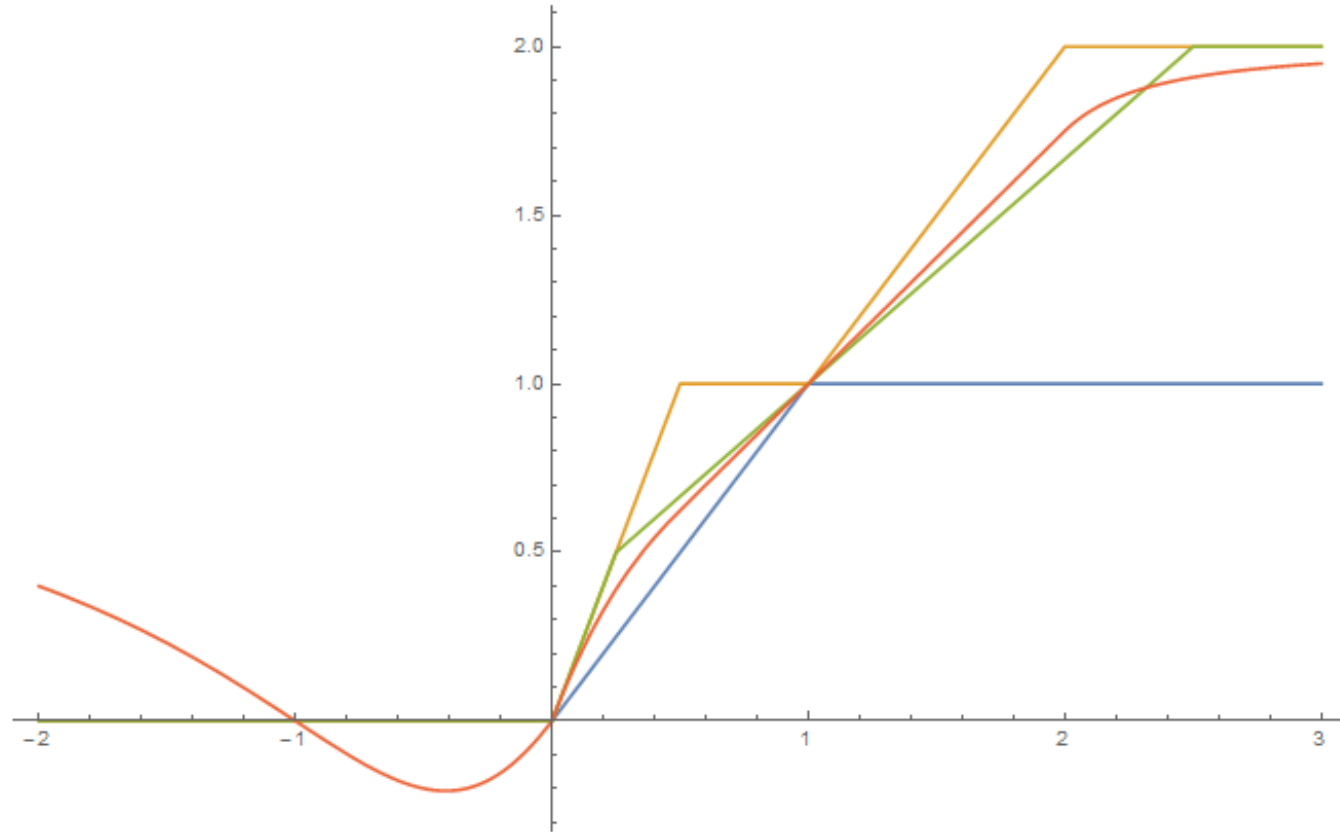


Limiters



Superbee, Minmod

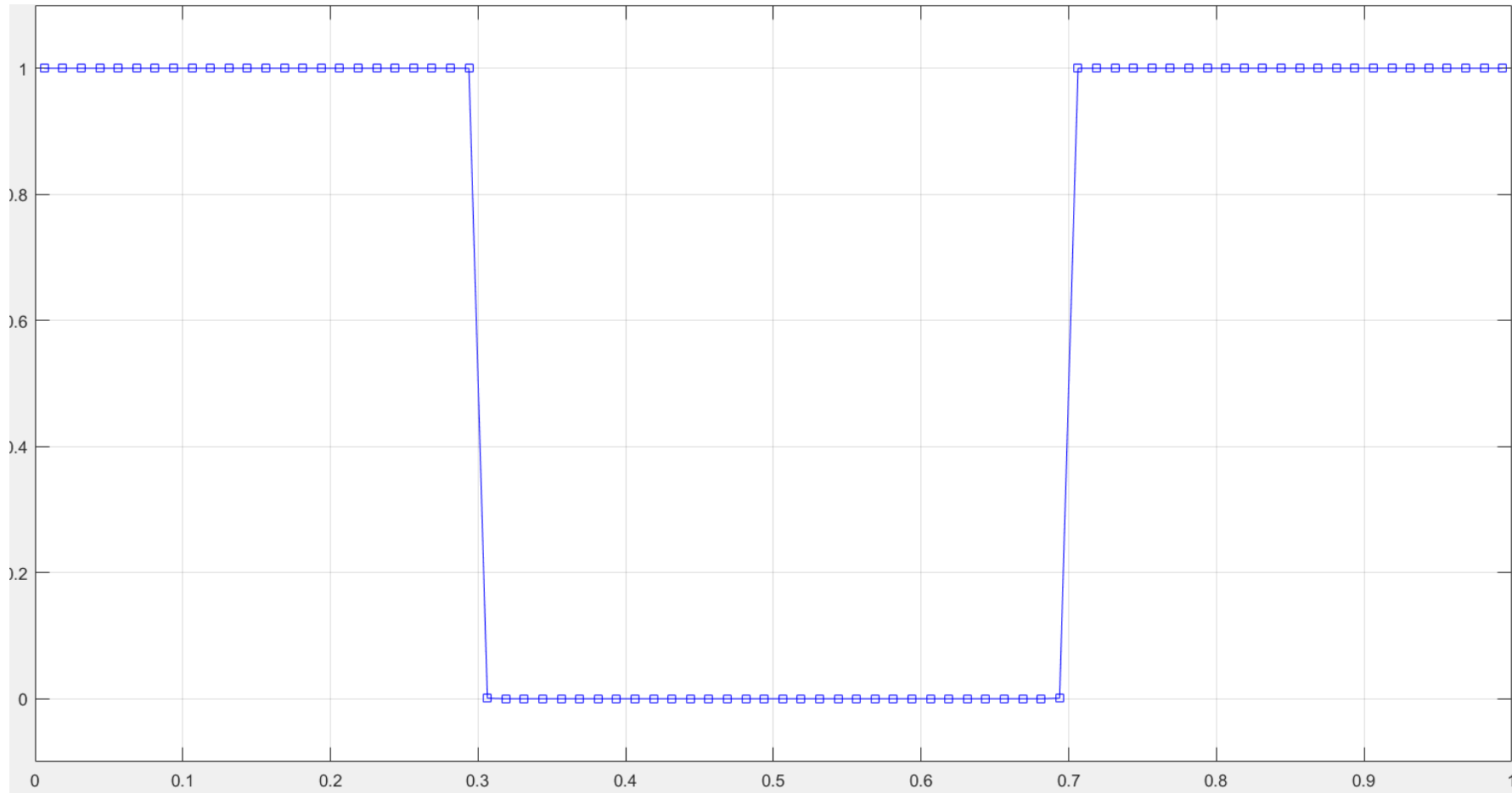
Limiters



Superbee, Minmod, Koren, TCDF

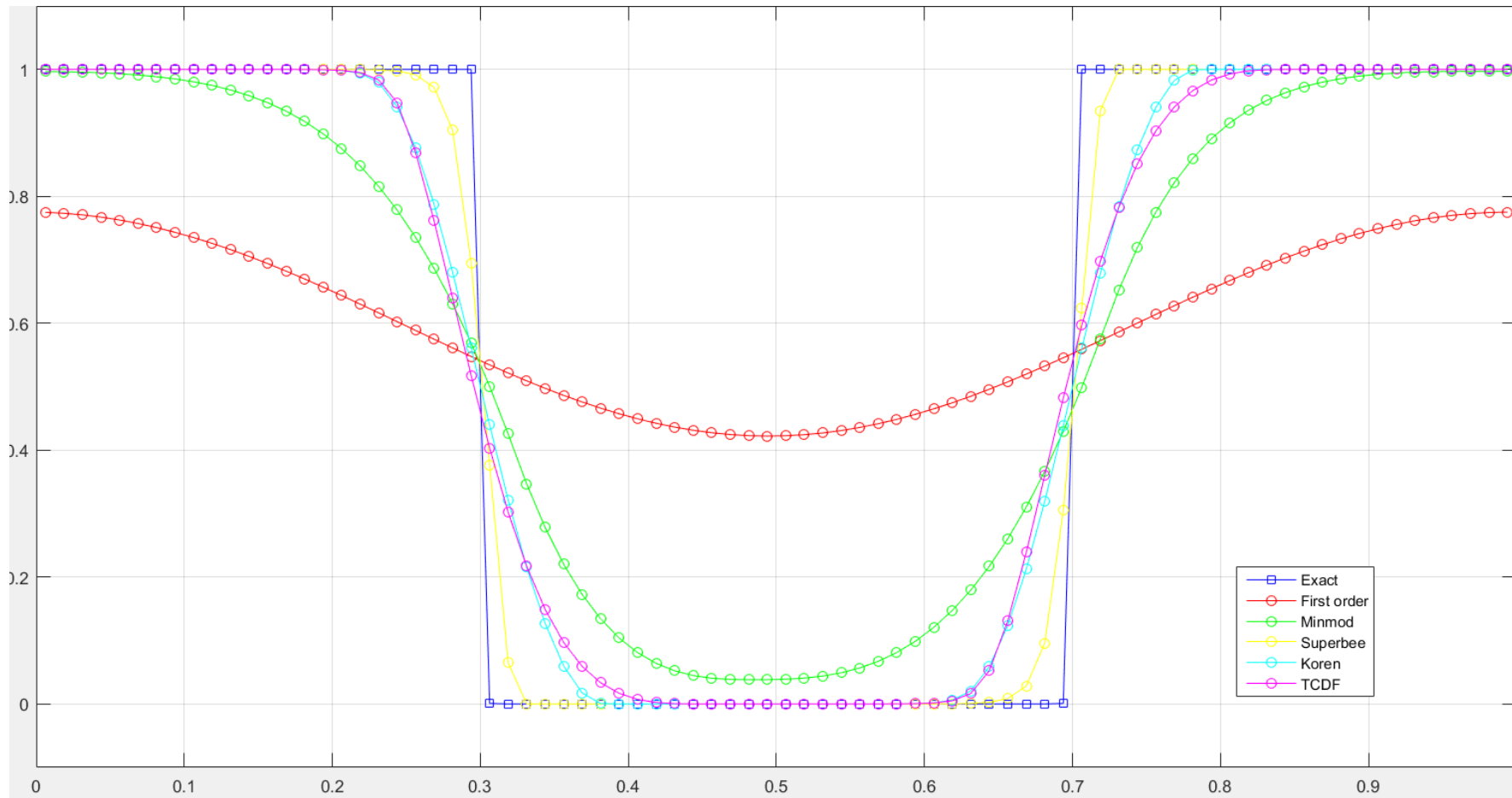
Comparison of limiters

- 1D Linear advection equation:



Comparison of limiters

- 1D Linear advection equation:



Riemann solver

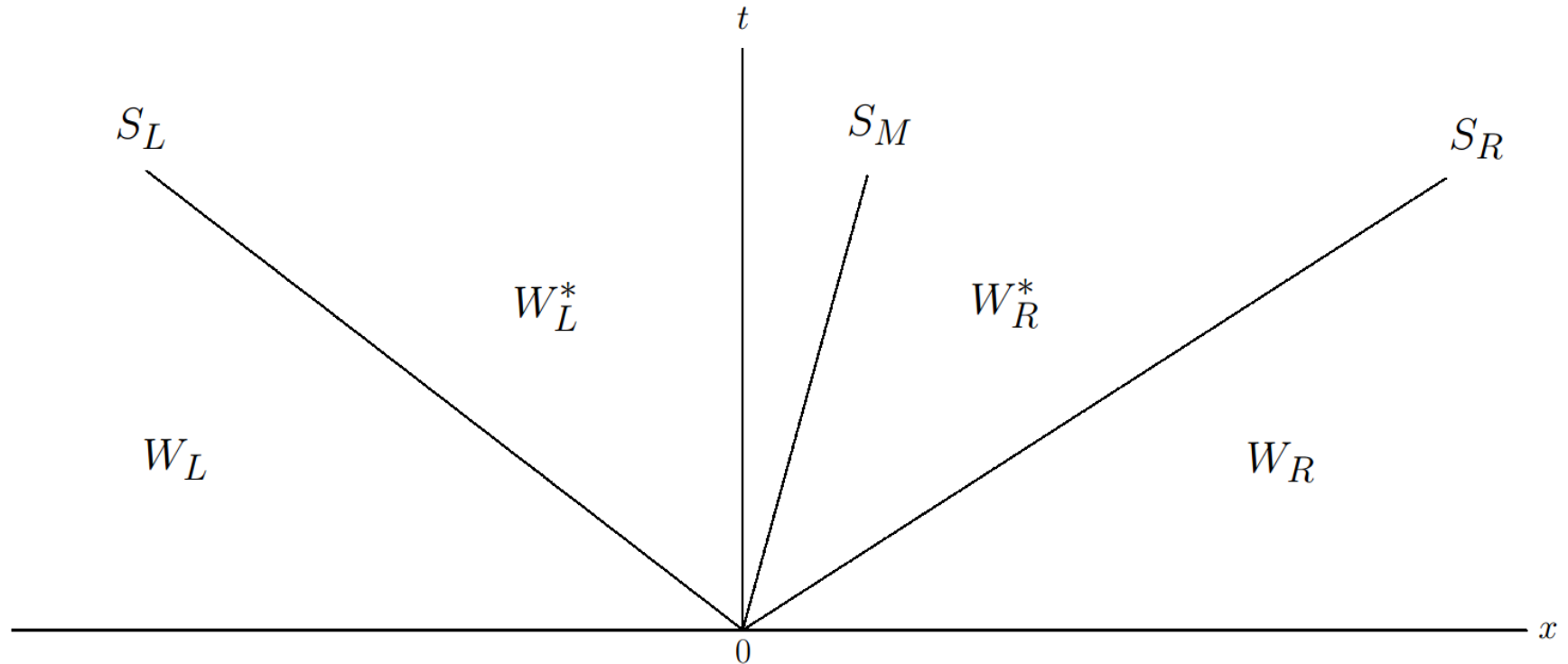
HLLC approx. Riemann solver

Wave speed estimates: S_L, S_M, S_R

Constant intermediate states

Positivity preserving

Shock waves are resolved exactly



Non-conservative terms

$$(\alpha)_t + (\alpha u)_x = (\alpha - \varphi)(u)_x,$$

HLLC type way

$$\Delta t \mathbf{S}_{x,i,j}^n = (\alpha_{i,j} - \varphi_{i,j}) (u_{i+\frac{1}{2},j}^* - u_{i-\frac{1}{2},j}^*)_x$$

u^* taken as the HLLC advection speed

$$u^* = \begin{cases} u_L, & S_L, S_M, S_R > 0 \\ \frac{S_L - u_L}{S_L - S_M} S_M, & S_R, S_M > 0, S_L < 0 \\ \frac{S_R - u_R}{S_R - S_M} S_M, & S_R > 0, S_L, S_M < 0 \\ u_R, & S_L, S_M, S_R < 0 \end{cases}$$

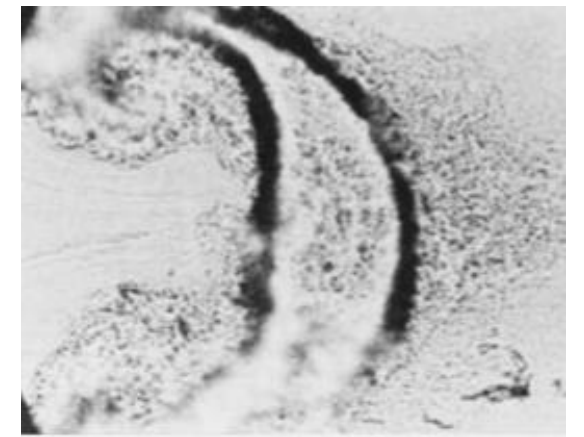
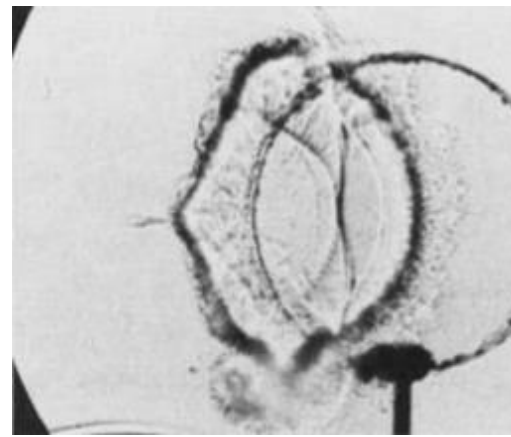
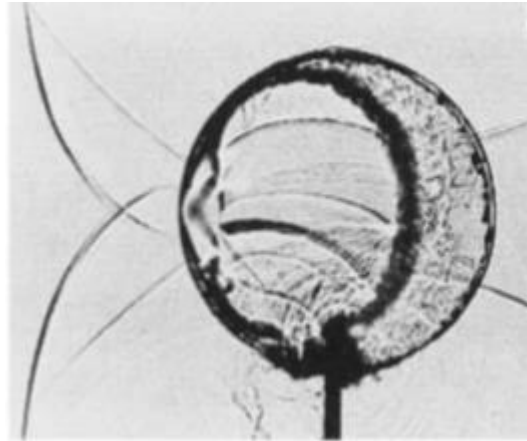
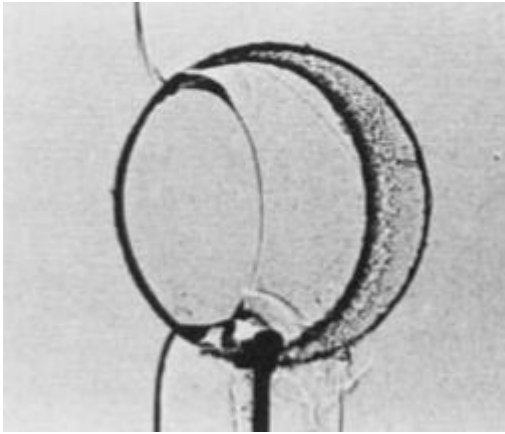
Time integration

TVD 3rd order Runge Kutta explicit time integration

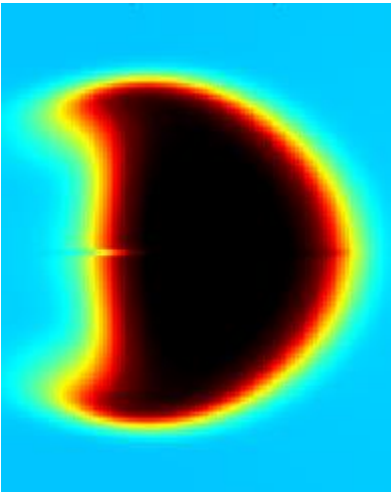
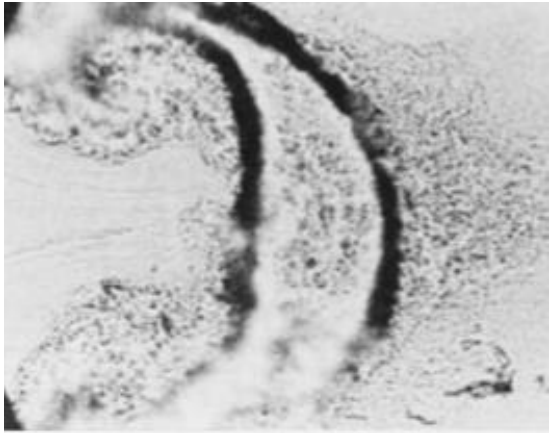
Time step: CFL condition:

$$\Delta t \leq \frac{1}{4} \min(\Delta x / u_{max}, \Delta y / v_{max},)$$

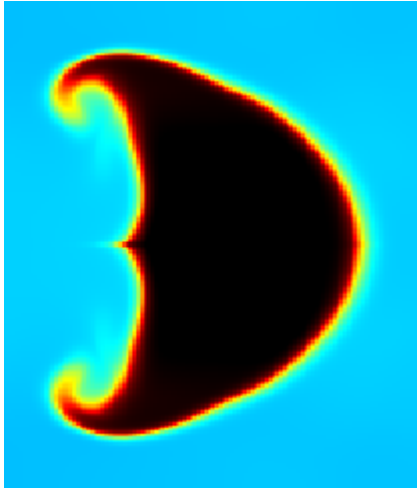
Haas and Sturtevant (1)



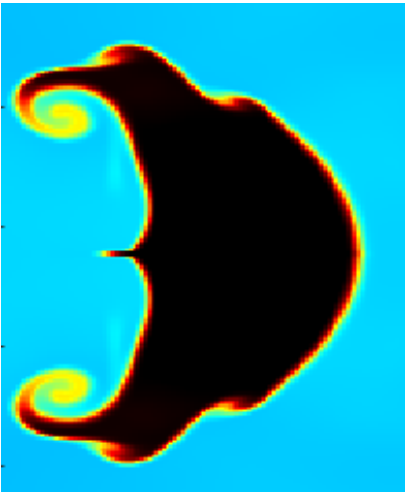
Haas and Sturtevant (1)



First order



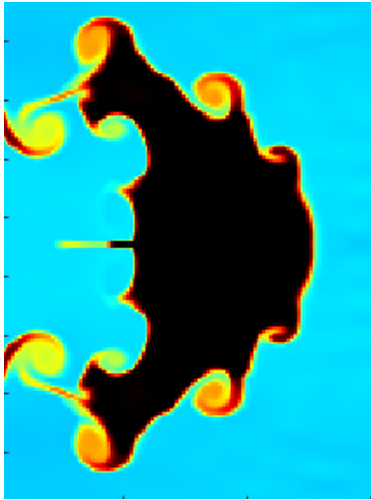
Minmod



Koren

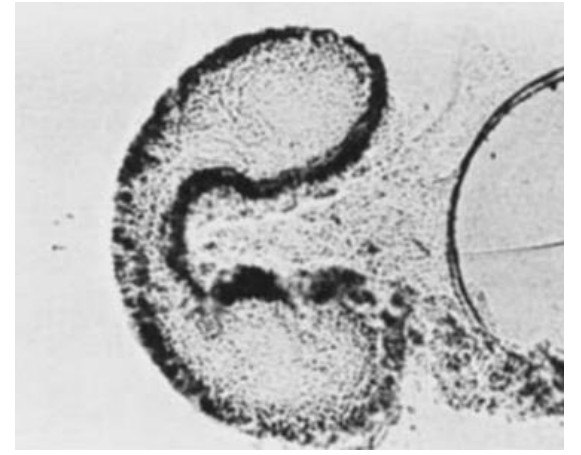
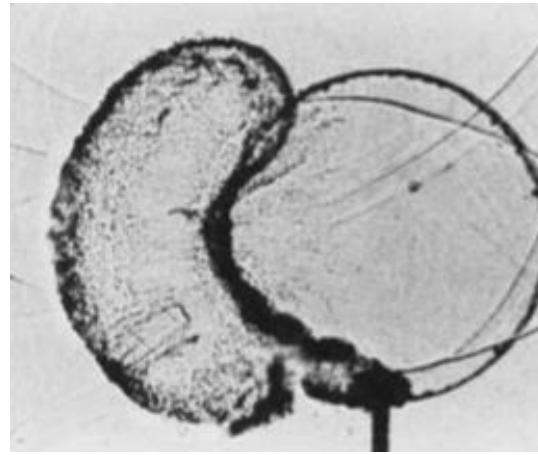
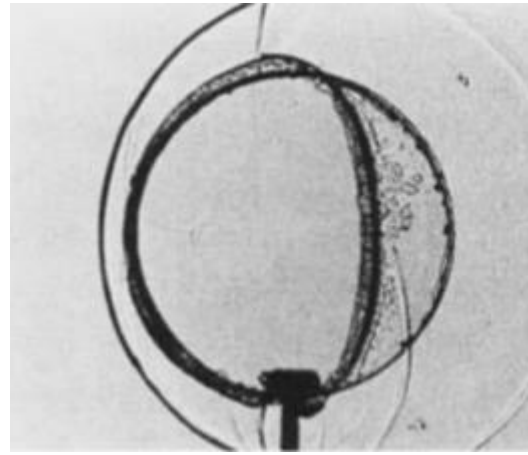
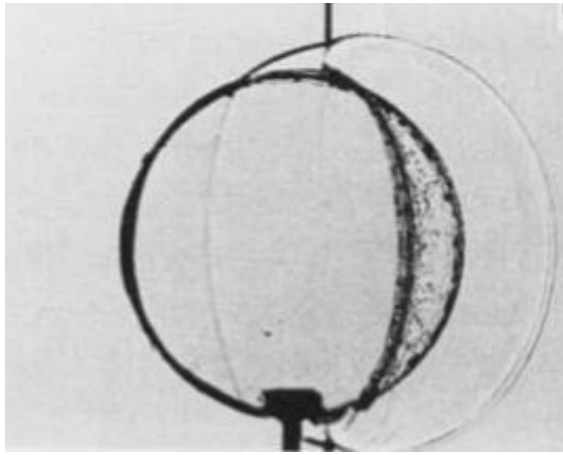


TCDF

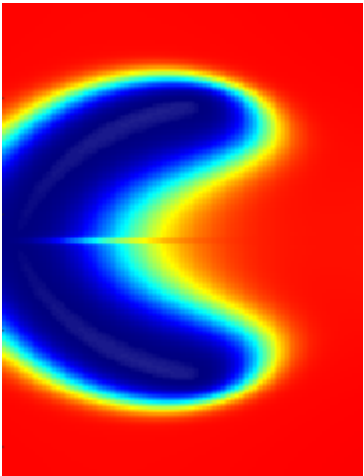
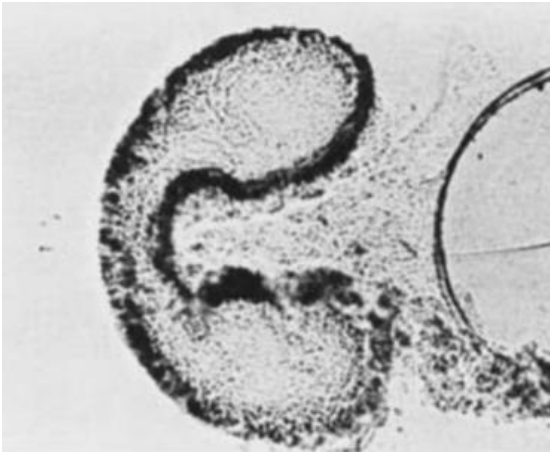


Superbee

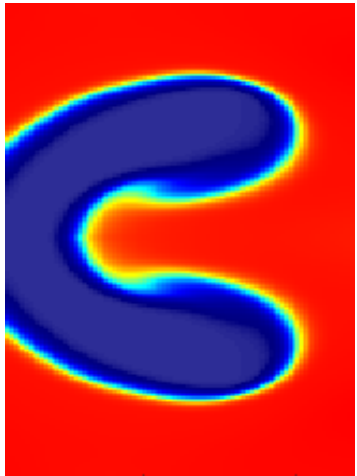
Haas and Sturtevant (2)



Haas and Sturtevant (2)



First order



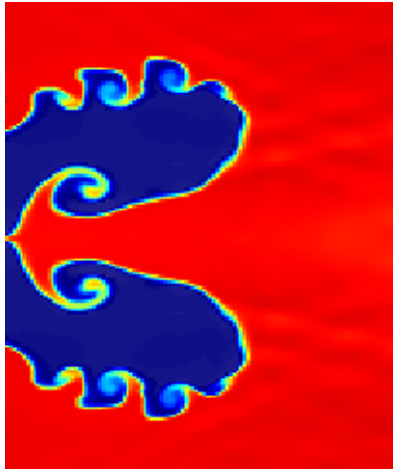
Minmod



Koren



TCDF



Superbee

Spatial reconstruction

Theory well developed for simple cases

But in this case

- 2D
- System of equations
- Non-linear equations
- Source terms
- 3rd order time integration